

# APPLICATION UNDER UNITED STATES PATENT LAWS

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Invention: PROCESS FOR THE PREPARATION OF AN IMPACT-RESISTANT POLYMER COMPOSITION

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## This is a:

- ☐ Provisional Application
- ☐ Regular Utility Application
- ☒ Continuing Application
  - ☒ The contents of the parent are incorporated by reference
- ☐ PCT National Phase Application
- ☐ Design Application
- ☐ Reissue Application
- ☐ Plant Application
- ☐ Substitute Specification
  - Sub. Spec Filed \_\_\_\_\_
  - in App. No. \_\_\_\_\_ / \_\_\_\_\_
- ☐ Marked up Specification re
  - Sub. Spec. filed \_\_\_\_\_
  - In App. No. \_\_\_\_\_ / \_\_\_\_\_

## SPECIFICATION

PROCESS FOR THE PREPARATION OF AN IMPACT-RESISTANT5 POLYMER COMPOSITION

The invention relates to a process for the preparation of an impact-resistant polymer composition  
10 containing 0.5-75 parts by weight of a rubber composition (per 100 parts by weight of the matrix polymer).

Such compositions are known from, inter alia, US-A-4,174,358 and this patent publication  
15 discloses various processes for the preparation of these compositions. These processes all essentially comprise a rubber functionalization step followed by incorporation of the functionalized rubber in the desired concentration into the matrix polymer.

20 These state-of-the-art polymer compositions in general exhibit a good impact resistance, which is determined, inter alia, to an important degree by the rubber content of the composition. However, the presence of the rubber composition causes the stiffness  
25 to decrease and the creep to increase.

For applications in which no or only minimal creep is allowed while a good impact resistance is required, for instance in plastic hammer heads, it is therefore necessary to have a polymer composition  
30 that possesses this combination of conflicting properties. Another application in which this combination of properties is required is that of plastic profiles that serve as heat bridge in metal window and door profiles and screw plugs, where

toughness is required for assembly purposes while no creep may occur when the materials are subsequently subjected to a permanent load. Compositions obtained by the state-of-the-art process, however, cannot fully  
5 meet this requirement.

The aim of the invention therefore is a process for the preparation of an impact-resistant polymer composition that has an excellent impact resistance at no or only minimal creep.

10 This aim is achieved by melt mixing of a matrix polymer A with a composition comprising a dispersed rubber composition in a matrix polymer B, the dispersed rubber composition in matrix polymer B having been obtained by melt mixing of matrix polymer B with a  
15 rubber composition that contains at least one non-functionalized rubber and one functionalized rubber, in such amounts that the desired rubber concentration in the impact-resistant polymer composition is reached.

Also part of the invention are the  
20 composition obtainable by the process according to the invention and the products obtained from the composition according to the invention as well as the (granule) mixture of matrix polymer A and the dispersed rubber composition in matrix polymer B as needed for  
25 the process of the invention.

Matrix polymer A can in principle be chosen freely, but the process according to the invention offers advantages if polymer A is chosen from the group consisting of polyamides, polyesters, polyacetals and  
30 polycarbonates. The invention is effective in particular if polymer A is a polyamide or a polyester.

For matrix polymer B in principle any

polymer can be chosen that can suitably be mixed with polymer A and in which the rubber composition can suitably be dispersed. Preferably, polymer B is chosen from the group consisting of polyamides, polyesters, polyacetals and polycarbonates. Even more preferably, polymers A and B are of the same type of polymer, for instance A and B are both polyamides, for instance an aliphatic and a semi-aromatic polyamide. Most preferably, A and B are identical.

The rubber composition dispersed in polymer B comprises at least one non-functionalized rubber and at least one functionalized rubber. Rubber is here understood to mean a polymeric compound with a glass transition temperature lower than 0°C, preferably lower than -20°C, most preferably lower than -40°C.

A rubber is called functionalized when it contains groups that can react with matrix polymer B and/or A.

Examples of polymers covered by the definition of rubber are copolymers of ethylene and  $\alpha$ -olefins, for instance ethylene-propylene rubbers. Very suitable for use in the process according to the invention are the so-called plastomers based on ethylene and C4-C12 olefins, for instance octene, and produced using a metallocene catalyst.

Other rubbers that can suitably be used in the process according to the invention are styrene-butadiene based block copolymers.

Functional groups can be introduced into the rubber in many ways. A great many preparation methods and examples of these functionalized rubbers are described, for instance, in the above-mentioned US

patent publication US-A-4,174,358. Several of these functionalized rubbers are commercially available under different names. Very suitable are rubbers that are chemically modified by reaction with maleic anhydride or by graft polymerization of the rubber with an unsaturated dicarboxylic anhydride or an unsaturated dicarboxylic acid or an ester thereof, for instance maleic anhydride, itaconic acid and itaconic anhydride, fumaric acid and maleic acid or a glycidyl acrylate, for instance glycidyl methacrylate, and vinyl alkoxysilane. The functional groups are highly reactive relative to, inter alia, amino end groups in polyamides, hydroxyl end groups in polyesters and acid end groups in both polyamides and polyesters.

The content of compounds supplying functional groups in the functionalized rubber may vary within wide limits, for instance between 0.01 and 5 wt.%. The best results are generally achieved with a content between 0.3 and 3 wt.%.

The weight ratio of non-functionalized to functionalized rubber may vary within wide limits and is determined in part by the functional groups content of the rubber and the available reactive groups in the matrix polymer. One skilled in the art can determine this by means of simple experiments. In general, this ratio will be between 10 and 0.1, preferably between 5 and 0.1.

The rubber composition content of the composition with matrix polymer B may vary within wide limits, for instance between 20 and 70 wt.%, calculated on the total weight of rubber composition + polymer B, preferably the rubber composition content is chosen as

high as possible, for instance higher than 30 wt.%, more preferably higher than 40 wt.%. Very good results are achieved with contents of at least 50 wt.% or higher.

5                   The non-functionalized rubber and the rubber that is functionalized may be identical or different. Combinations are for instance possible of an ethylene- $\alpha$ -olefin copolymer and the same ethylene- $\alpha$ -olefin copolymer modified with, for instance, maleic  
10                   anhydride. The same ethylene- $\alpha$ -olefin copolymer may also be combined with, for instance, an acid-modified styrene-butadiene tri-block copolymer.

                  Particularly good results are achieved with the process according to the invention when the rubber  
15                   composition in matrix polymer B is present in finely dispersed particles. Preferably, the dispersed particles of the rubber composition are then built up of a core of non-functionalized rubber and a shell of functionalized rubber.

20                   The composition of matrix polymer B with the rubber composition can be obtained by melt mixing of the constituent components. In doing so, use is preferably made of high shear forces and the conditions are chosen so that the viscosity in the melt of the  
25                   rubber phase is higher than that of the polymer matrix. During the melt mixing process crosslinking of the rubber phase may optionally take place. However, a non-crosslinked rubber is preferred. Non-crosslinked rubber is here understood to be a rubber that is substantially  
30                   not crosslinked. In practice, however, some degree of crosslinking can hardly be avoided during melt mixing at the high temperatures then prevailing. The resulting

gel content will be lower than 50 wt.%, preferably lower than 30 wt.%, even more preferably lower than 10 wt.%. The gel content is here defined as the rubber fraction that is insoluble in the solvent that is suitable for the rubber in question. For ethylene-propylene copolymer rubbers, for instance, this solvent is xylene. When reference is made to crosslinking of the rubber composition, this is understood to mean the melt mixing process carried out in the presence of a vulcanization agent, for instance a peroxide.

Optionally, the rubber composition can first be crosslinked during incorporation of the composition into matrix polymer A. This process has the advantage that it can be performed under milder and better controllable conditions, so that less damage is done to the matrix polymer, while the process also has the advantage that mechanical properties can be adapted from case to case on the basis of similar compositions.

For mixing in the melt phase the customary techniques and equipment can be employed. Particularly suitable for production of the composition in polymer matrix B is, for instance, a co-rotating twin-screw extruder, while for mixing in of the composition into matrix polymer A in many cases a single-screw extruder, which may be directly prearranged in the injection moulding process, may suffice. Preferably, the mixing operations in the melt are carried out under an inert gas atmosphere.

During melt mixing optionally the customary additives and auxiliary materials for the polymer compositions can be added, for instance stabilizers, colourants, processing aids, for instance release

agents, flame-retardant additives and fillers or reinforcing (fibre) materials. Preferably, the additives and auxiliary materials are introduced into the melt only after the rubber composition has been  
5 dispersed in the matrix polymer.

Most preferably, the auxiliary materials and additives are added to the melt of polymer A, optionally simultaneously with the mixing in of the composition of polymer matrix B or separate therefrom.

10 The invention will now be elucidated on the basis of the following examples and comparative examples.

Materials:

15	AKULON® F235C	polyamide-6, rel. visc. 2.3, from DSM
	AKULON® 223 TP4	blend of polyamide 6 and Excellor® (80:20) from DSM, Netherlands
	AKULON® K 120	Polyamide-6, rel. visc. 2.2, from DSM
20	EXXELOR®	ethylene-propylene rubber modified with 0.7 wt.% maleic anhydride from Exxon, USA
	KRATON® FG 1901X	styrene-butadiene block copolymer, modified with 2 wt.% maleic anhydride from Shell, Netherlands
25	EXACT® 8201	ethylene-octene copolymer from DEX PLASTOMERS, Netherlands
	EXACT® MA	Maleic acid modified ethylene-octene copolymer, 0.9 wt.% MA
30		



### Examples and comparative experiments

The above-mentioned materials were used to produce the compositions listed in Table 1.

5 All compositions were obtained by premixing the components in the solid phase and subsequently feeding them to a twin-screw extruder and mixing them using a temperature profile of 150 to 260°C.

10 The properties of compositions 2, 4, 6, 8, 10, 11 and 13 were compared (compositions 6, 8, 10 according to the process of the invention, the other ones being comparative experiments).

#### Points examined:

- 1) The morphology, in particular the appearance and the particle size in the rubber phase. To  
15 this end TEM, transmission electron microscopy, pictures were made.
- 2) The mechanical behaviour, specifically the impact resistance (Izod, notched) and the creep  
behaviour on the basis of practical tests.

20 Morphology: The rubber phase in compositions 2, 4, 6, 8, 10 and 13 was dispersed in the polyamide matrix. Composition 11 had 2 rubber phases, viz. very fine Kraton particles < 100 nm and larger EXACT® particles, the diameter of which varied between  
25 0.5 and 2 µm. These particles were generally provided with a very thin shell of KRATON® FG. In composition 10 all KRATON® FG was present in the shell around the EXACT® particles, which were present in a particle size of about 0.1 - 0.6 µm.

30 In all cases in which a combination of functionalized rubber and a non-functionalized rubber was applied, the particles in the rubber phase were

observed to have a distinct sphere-shell structure.

Example 1 and comparative Experiment A

Bars with a diameter of 8 cm were extruded  
5 from composition 10 and composition 2. From these bars,  
hammer heads were machined, which were attached to a  
wooden stem by means of a pin. The hammer head obtained  
from composition 2 after some time exhibited play  
relative to the stem (comp. Exp. A), while the head  
10 from composition 10 (Example 1) was still firmly  
attached after 14 days of testing.

Example 2 and comparative Experiment B

From compositions 2, 4, 6, 8, 10 and 11  
15 plugs for attaching screws in brickwork were injection  
moulded. After the plugs had been placed in a series of  
uniform holes and screws had been inserted, the force  
needed to draw the plug with the screw out of the hole  
was measured after fixed intervals. The results are  
20 outlined in Table 1.

- does not meet the standard set  
o meets the standard set  
+ more than meets the standard set

The plugs from compositions 2, 4 and 11  
25 (not according to the invention) are found to 'set'  
more rapidly, i.e. exhibit higher creep and can sooner  
be drawn out of the hole than the plugs from  
compositions 6, 8 and 10 according to the invention.

Table 1

Composition, parts by weight	1	2	3	4	5	6	7	8	9	10	11	12	13
AKULON® F 235C	100	75		90		90		90		90	95		90
AKULON® K 120			50		50		50		60			50	
AKULON® TP4	-	25											
EXXELOR®	-		50		20								
KRATON® FG	-								10		1		
C8-EXACT®	-						40		40		4		
C8-EXACT® MZA	-						10					50	
Composition 3				10									
Composition 5						10							
EPDM					30								
Composition 7								10					
Composition 9										10			
Composition 12													10
particle size [µm]	n.a.	0.4-2		0.5-4		0.5-3		0.4-		0.1-	0.3-		0.5-
								1.6		0.6	1.5		3.0
IZOD notched 23°C	7.2	12.8	NB	12.5	NB	13.0	NB	13.5	NB	13.0	11.8	NB	12.4
[kJ/m²]													
creep		-		-		0		+		+	-		+